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GB A 2137348 GB 1555549 GB 0809681 GB A 2128326 GB 1531729 EP A2 0028114 GB A 2076536 GB 1372724 US 4320659 **GB A 2019558** GB 0873538 US 4203324

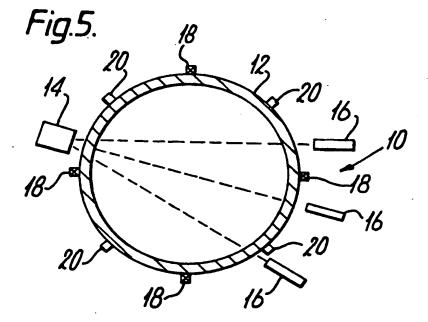
(58) Field of search

G1A

Selected US specifications from IPC sub-classes G01F **G01N**

(54) Pipeline inspection

(57) The nature of the flow pattern in a pipeline carrying both a liquid and a gas is characterised by measuring the void fraction or the average density along at least one chord across the pipeline (12) and by determining the distribution of liquid around the periphery of the pipe wall. The average density or void fraction may be measured by the absorption of gamma rays from a source (14); while the peripheral distribution may be determined from the attenuation of ultrasonic plate waves propagating through sectors of the wall between transmitters (18) and receivers (20), whereby the presence or absence of liquid is detected.



68 15C

Fig.1.

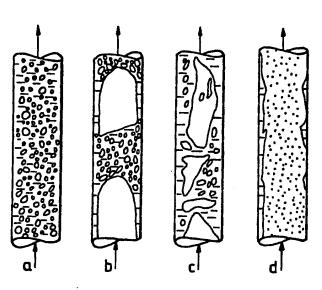


Fig.2.

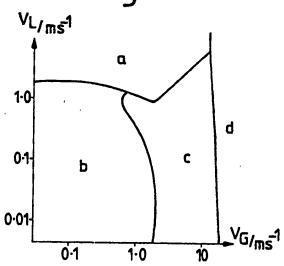
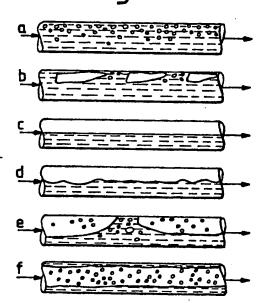
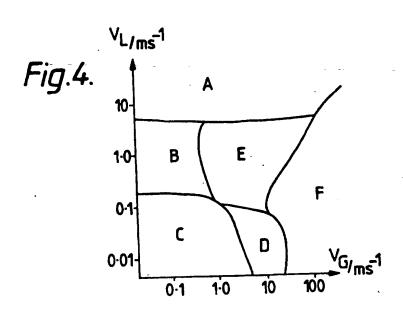
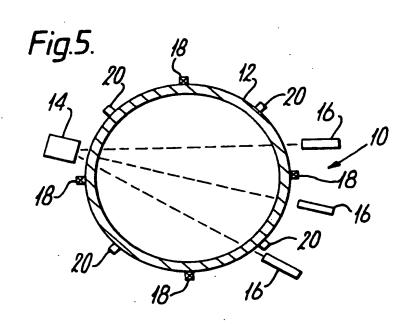


Fig. 3.







SPECIFICATION

Pipeline inspection

5 The invention relates to a method and an apparatus for the inspection of pipelines to obtain information about their contents.

The invention is particularly applicable to the inspection of pipelines carrying both a gas and 10 a liquid, in which the nature of the flow depends upon the flow rates of the two components, ranging from small bubbles of gas dispersed in the liquid, to a thin peripheral layer of liquid around the wall of the pipeline.

15 According to the present invention there is provided a method of inspection of a pipeline carrying a liquid to characterise the contents thereof, the method comprising measuring the average density along at least one chord 20 across the pipeline, and determining the distribution of liquid around the periphery of the pipeline.

The average density is preferably measured along a plurality of chords across the pipeline; 25 and can be measured from the attenuation of gamma rays, X-rays or neutrons.

The peripheral distribution of the liquid is preferably determined by detecting the presence or absence of liquid at a plurality of loca-30 tions around the periphery of the pipeline. This may be achieved using ultrasonic waves; either by causing ultrasonic compression waves to propagate through the wall of the pipeline and detecting the amplitude of the 35 wave reflected at the inner surface of the wall; or by causing ultrasonic plate waves to propagate from a transmitter along a portion of the wall, circumferentially or axially, and detecting the amplitude of the wave received at 40 a receiver spaced apart from the transmitter.

The invention also provides an apparatus for performing the method of inspection.

The invention will now be further described by way of example only and with reference to 45 the accompanying drawings, in which:

Figures 1a to 1d show diagrammatically flow patterns which can occur in a vertical pipeline;

Figure 2 shows graphically the gas and 50 liquid flow velocities at which the flow patterns of Figs. 1a to d occur;

Figure 3a to 3f, show diagrammatically flow patterns which can occur in a horizontal pipe;

Figure 4 shows graphically the gas and 55 liquid flow velocities at which the flow patterns of Figs. 3a to f, occur;

Figure 5 shows diagrammatically an apparatus for inspection of a pipeline.

When a gas-liquid mixture flows in a pipel-60 ine the two phases may define one of a variety of different patterns, the particular pattern depending on the physical properties of the liquid and the gas, the dimensions of the pipeline, and the flow rates of the two

65 phases. The flow patterns are described for

example in an article by Y. Taitel and A. E. Dukler, in A. I. Ch. E. Journal Vol. 22, No. 1 (January 1976); and an article by Y. Taitel, A. E. Dukler and D. Bornea in A. I. Ch. E. Journal 70 Vol. 26, No.3 (May 1980).

Referring to Figs. 1a to d, the typical flow patterns where the gas and liquid flow upwardly in a verticle pipeline are shown. Fig. 1a shows "Bubble flow", in which the gas phase 75 is distributed as discrete bubbles in a continous liquid phase. Fig. 1b shows "Plug flow", in which most of the gas forms large bulletshaped bubbles almost as wide as the pipeline. Between these large bubbles and the wall 80 is a thin liquid film falling downwards. Fig. 1c shows "Churn flow", in which the flow is much more chaotic, parts of the liquid phase alternating in their direction of flow and churn-

ing around. Fig. 1d shows "Annular flow" which is characterised by the continuity of the gas phase along the centre of the pipeline, and in which the liquid phase forms a thin film on the wall, with a wavy surface. Parts of the liquid phase may be in the form of droplets 90 entrained in the gas, and in some circumstances these may form long foamy wisps.

Referring to Fig. 2 this indicates graphically the flow rates at which the flow patterns of Fig. 1 may occur, the graph axes representing 95 the liquid superficial velocity (V_I) and the gas superficial velocity (V_a) , and the letters a to d corresponding to the flow patterns of Figs. 1a to d respectively (see May 1980 reference above). The superficial velocity means the 100 volumetric flow rate divided by the cross-sectional area of the pipeline.

Referring to Figs. 3a to f, typical flow patterns are shown for a horizontal pipeline; and Fig. 4 indicates graphically the superficial velocities V_i and V_g at which the flow patterns of Fig. 3 may occur (see January 1976 reference above). The letters A to F in Fig. 4 correspond to the flow patterns of Figs. 3a to f, respectively. Fig. 3a shows "Bubble flow", 110 similar to that of Fig. 1a except that the bubbles of gas tend to flow in the upper part of the pipeline. Fig. 3b shows "Plug flow" similar to that of Fig. 1b. Fig. 3a shows"Stratified flow", in which the liquid and gas phases are completely separate, and the interface is smooth. At higher gas velocities waves begin to form on the liquid surface, forming "Wavy flow" as shown in Fig. 3d,

and at still higher gas velocities some of the waves become large enough to reach the top of the pipeline, forming "Slug flow" as shown in Fig. 3e. These large waves or slugs are often frothy, and move along with the gas at high velocity. Fig. 3f, shows "Annular flow", which occurs at still greater gas velocities and

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is similar to that of Fig. 1d, differing in that the liquid film tends to be thicker at the bottom of the pipeline than the top.

The flow patterns described above have 130 hitherto principally been studied using optical

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techniques, in transparent pipelines. Such techniques are obviously inapplicable to practical pipelines for example for oil and natural gas mixtures, which are of steel with a wall 5 thickness of over 10mm.

Referring now to Fig. 5, an apparatus 10 is shown for characterising the nature of the flow inside a pipeline 12, the pipeline 12 being shown in cross-section. The apparatus 10 10 comprises a gamma ray source 14 arranged to cause three beams of gamma rays to traverse the pipeline 12 along respective chords (shown as broken lines), and three gammaray detectors 16 arranged to detect the rays 15 after their passage through the pipeline 12. The apparatus 10 also comprises four ultrasonic transmitters 18 and four ultrasonic receivers 20 mounted on the outside of the pipeline 12 equally spaced around its circumfer-20 ence, each receiver 20 being midway between two transmitters 18. Each transmitter 18 when energised causes ultrasonic plate waves (similar to a Lamb wave) to propagate in both directions around the wall of the pipeline 12, 25 to be detected by the adjacent receivers 20. If a liquid layer of thickness greater than a few millimeters is present on the portion of wall through which propagation of the plate waves is taking place then mode conversion of the 30 waves will occur, compression waves being generated in the liquid and the amplitude of the plate wave decreasing to zero within a propagation distance of a few wavelengths.

in operation of the apparatus 10 the gamma 35 ray source 14 produces the three beams continuously and each of the three detectors 16 gives a continuous indication of the degree of absorption along the respective chord, and hence of the average density (or the void frac-40 tion) of the pipeline contents along the chord. Diametrical pairs of transmitters 18 are excited alternately, the amplitude of the signals detected by the receivers 20 indicating the presence or absence of a liquid layer on the por-45 tion of pipeline wall between the transmitter 18 and the receiver 20. Inspection of the indications given by the gamma ray detectors 16 and those given by the ultrasonic receivers 20 thus enables the distribution of liquid and gas

50 within the pipeline 12, and its temporal variations, and so the nature of the flow pattern, to be determined. The apparatus 10 is noninvasive, and involves no modifications to the pipeline 12 itself, and so is applicable to prac-55 tical pipe lines 12.

It will be appreciated that the number of chords along which the degree of absorption is measured might be fewer or more than three; that the orientation of the chords might 60 be different from those shown in the Fig; and that the source 14 of gamma rays might be replaced by a source of x-rays or neutrons, the detectors 16 being changed accordingly.

It will be further appreciated that the num-65 bers of ultrasonic transmitters 18 and receiv-

ers 20 might differ from that described; and the transmitters 18 might be arranged to cause the plate waves to propagate along the length of the pipeline 12 rather than circumfer-70 entially, the receivers 20 being repositioned accordingly.

A modification of the apparatus 10 includes two sets of transmitters 18 and receivers 20 spaced apart along the pipeline 12. Correlation 75 of the indications given by the two sets enables the rate of movement of, for example, a liquid plug along the pipeline to be determined.

80 CLAIMS

1. A method of inspection of a pipeline carrying a liquid to characterise the contents thereof, the method comprising measuring the average density along at least one chord 85 across the pipeline, and determining the distribution of liquid around the periphery of the pipeline.

2. A method as claimed in Claim 1 wherein the average density is measured along 90 a plurality of chords across the pipeline.

3. A method as claimed in Claim 1 or Claim 2 wherein the peripheral distribution of the liquid is determined by detecting the presence or absence of liquid at a plurality of loca-95 tions around the periphery of the pipeline.

4. A method as claimed in Claim 3 wherein the peripheral distribution is determined by causing ultrasonic compression waves to propagate through the wall of the pipeline and detecting the amplitude of the wave reflected at the inner surface of the wall.

A method as claimed in Claim 3 wherein the peripheral distribution is deter-105 mined by causing ultrasonic plate waves to propagate from a transmitter along a portion of the wall, and detecting the amplitude of the wave received at a receiver spaced apart from the transmitter.

6. A method of inspection of a pipeline 110 carrying a liquid to characterise the contents thereof substantially as hereinbefore described with reference to, and as shown in, Fig. 5 of the accompanying drawings.

7. Apparatus for inspecting a pipeline car-115 rying a liquid to characterise the contents thereof, comprising means for measuring the average density along at least one chord across the pipeline, and the means for deter-120 mining the distribution of liquid around the periphery of the pipeline.

8. Apparatus for inspecting a pipeline carrying a liquid to characterise the contents thereof substantially as hereinbefore described 125 with reference to, and as shown in, Fig. 5 of the accompanying drawings.

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